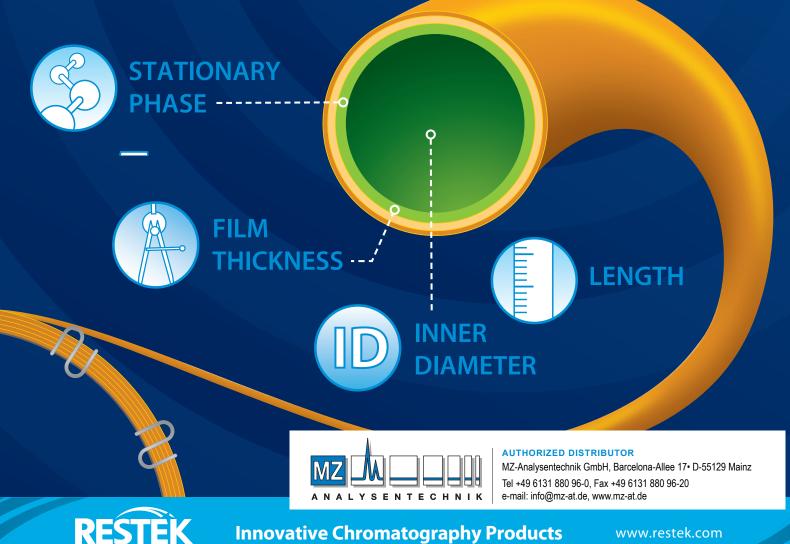
Guide to GC Column Selection and Optimizing Separations



WHICH COLUMN DO I NEED?

- Learn how to choose the right column the first time.
- Optimize separations for the best balance of resolution and speed.
- Troubleshoot quickly and effectively based on chromatographic symptoms.



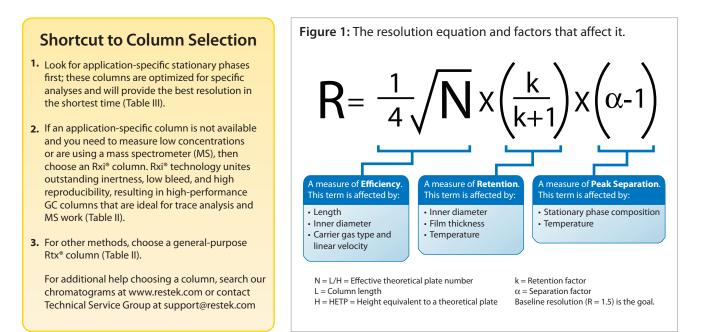


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WHICH COLUMN DO I NEED? Resolution Equation—The Key to Column Selection and Optimizing GC Separations

You can improve lab productivity by assuring that speed and resolution are optimized. One of the best ways to do this is to use the resolution equation (Figure 1) as the key to controlling your separations. This fundamental equation helps you choose the best column stationary phase, length, inner diameter (ID), and film thickness for your specific applications. Once you understand the basics of how resolution is related to column characteristics, optimizing your analysis for both separation and speed becomes easier. This GC column selection guide discusses the basics of separation and teaches you how to choose the right GC column!

Resolution is the goal of every chromatographer, but how much resolution is enough? Practically speaking, we need enough retention to get sharp symmetrical peaks that are baseline resolved from each other, but not too much retention, where retention times are too long and peaks start to broaden. To achieve this goal, we must consider the column and non-column factors that affect our "perfect separation". Only then can we work towards selecting the right column and optimizing GC separations and analysis speed. Now, let's consider separation factor (α), retention factor (k), and efficiency (N) in turn and how they can help you select the right column and optimize your separation.



Use Separation Factor (a) to Choose the Best Stationary Phase

Choosing the right stationary phase is the first step toward optimizing your GC separation. It is the most important decision you will make because separation factor (α) has the greatest impact on resolution, and it is strongly affected by stationary phase polarity and selectivity.

Stationary phase *polarity* is determined by the type and amount of functional groups in the stationary phase. When choosing a column, consider the polarity of both the stationary phase and your target analytes. If the stationary phase and analyte polarities are similar, then the attractive forces are strong and more retention will result. Greater retention often results in increased resolution. Stationary phase polarity strongly influences column selectivity and separation factor, making it a useful consideration when selecting a column.

Stationary phase *selectivity* is defined by IUPAC as the extent to which other substances interfere with the determination of a given substance. Selectivity is directly related to stationary phase composition and how it interacts with target compounds through intermolecular forces (e.g., hydrogen bonding, dispersion, dipole-dipole interactions, and shape selectivity). As methyl groups in the stationary phase are replaced by different functionalities, such as phenyl or cyanopropyl pendant groups, compounds that are more soluble with those functional groups (e.g., aromatics or polar compounds, respectively) will interact more and be retained longer,

 $R = \left(\frac{1}{4}\sqrt{N}\right) \times \left(\frac{k}{k+1}\right) \times \left(\alpha - 1\right)$



Table I: Kovat's retention indices for GC phases can be used to approximate selectivity.

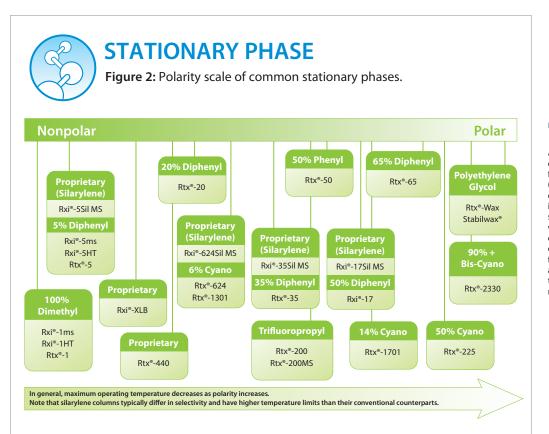
| Stationary Phase | Benzene | Butanol | Pentanone | Nitropropane |
|---|---------|---------|-----------|--------------|
| 100% Dimethyl polysiloxane | 651 | 651 | 667 | 705 |
| 5% Diphenyl/95% dimethyl polysiloxane | 667 | 667 | 689 | 743 |
| 20% Diphenyl/80% dimethyl polysiloxane | 711 | 704 | 740 | 820 |
| 6% Cyanopropylphenyl/94% dimethyl polysiloxane | 689 | 729 | 739 | 816 |
| 35% Diphenyl/65% dimethyl polysiloxane | 746 | 733 | 773 | 867 |
| Trifluoropropylmethyl polysiloxane | 738 | 758 | 884 | 980 |
| Phenyl methyl polysiloxane | 778 | 769 | 813 | 921 |
| 14% Cyanopropylphenyl/86% dimethyl polysiloxane | 721 | 778 | 784 | 881 |
| 65% Diphenyl/35% dimethyl polysiloxane | 794 | 779 | 825 | 938 |
| 50% Cyanopropylmethyl/50% phenylmethyl polysiloxane | 847 | 937 | 958 | 958 |
| Polyethylene glycol | 963 | 1,158 | 998 | 1,230 |

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In many cases, different GC oven temperature programs can change the elution order of sample analytes on the same column. Reconfirm elution orders if changing GC oven temperature programs.

often leading to better resolution and increased selectivity. In another example of the effect of stationary phase-analyte interactions, an Rtx*-200 stationary phase is highly selective for analytes containing lone pair electrons, such as halogen, nitrogen, or carbonyl groups, due to interactions with the fluorine pendant group in this phase. Selectivity can be approximated using existing applications or retention indices (Table I), making these useful tools for comparing phases and deciding which is most appropriate for a specific analysis.

Due to their influence on separation factor, polarity and selectivity are primary considerations when selecting a column. However, temperature limits must also be considered. In general, highly polar stationary phases have lower maximum operating temperatures, so choosing a column with the appropriate maximum operating temperature as well as optimal polarity and selectivity for the type of compounds being analyzed is crucial. Use Table II and Figure 2 determine which general-purpose column is most appropriate based on the selectivity, polarity, and the temperature requirements of your analysis. See Table III for a list of specialty stationary phases designed for specific applications.



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Any homologous series of compounds, that is, analytes from the same chemical class (e.g., all alcohols, all ketones, or all aldehydes, etc.) will elute in boiling point order on any stationary phase. However, when different compound classes are mixed together in one sample, intermolecular forces between the analytes and the stationary phase are the dominant separation mechanism, not boiling point.



| Restek | Phase Composition (USP Nomenclature) | Restek's Max Temps* | Agilent | Phenomenex |
|--------------------|--|------------------------|--|-----------------------|
| nester | mase composition (osr nomencature) | max remps | HP-1/HP-1ms. DB-1/DB-1ms. | I IICIIVIIICIICA |
| Rxi-1HT | | 400 °C | VF-1ms, CP Sil 5 CB, Ultra 1, | ZB-1, ZB-1MS, |
| Rxi-1ms, Rtx-1 | 100% Dimethyl polysiloxane (G1, G2, G38) | 350 °C | DB-1ht, HP-1ms UI, DB-1ms UI | |
| Rxi-5HT | | 400 °C | HP-5/HP-5ms, DB-5, Ultra 2, | ZB-5, ZB-5HT Inferno, |
| Rxi-5ms, Rtx-5 | 5% Diphenyl/95% dimethyl polysiloxane (G27, G36) | 350 °C | DB-5ht, VF-5ht, CP-Sil 8 CB | ZB-5ms |
| Rxi-5Sil MS | 5% (1,4-bis(dimethylsiloxy) phenylene/95% dimethyl polysiloxane | 350 °C | DB-5ms UI, DB-5ms, VF-5ms | ZB-5msi |
| Rxi-XLB | Proprietary Phase | 360 °C | DB-XLB, VF-Xms | MR1, ZB-XLB |
| Rtx-20 | 20% Diphenyl/80% dimethyl polysiloxane (G28, G32) | 320 °C | | MIKI, ZD-ALD |
| | 35% Diphenyl/65% dimethyl polysiloxane (G28, G32) | 320°C | — HP-35, DB-35 | |
| Rtx-35 | 55% Diprenyt/65% dimetriyt potysitoxane (642) | 320 C | , | ZB-35 |
| Rxi-35Sil MS | Proprietary Phase | 360 °C | DB-35ms, DB-35ms UI, VF-35ms | MR2 |
| Rtx-50 | Phenyl methyl polysiloxane (G3) | 320 °C | _ | _ |
| | | | DB-17ms, VF-17ms, | |
| Rxi-17 | 50% Diphenyl/50% dimethyl polysiloxane | 320 °C | CP Sil 24 CB | ZB-50 |
| | | | DB-17ms, VF-17ms, | |
| Rxi-17Sil MS | Proprietary Phase | 360 °C | CP Sil 24 CB | ZB-50 |
| Rtx-65 | 65% Diphenyl/35% dimethyl polysiloxane (G17) | 300 °C | - | - |
| | | | DB-624 UI, VF-624ms, | |
| Rxi-624Sil MS | Proprietary Phase | 320 °C | CP-Select 624 CB | ZB-624 |
| Rtx-1301, | | 280 °C | DB-1301, DB-624, CP-1301, | 70 (0) |
| Rtx-624 | 6% Cyanopropylphenyl/94% dimethyl polysiloxane (G43) | 240 °C | VF-1301ms, VF-624ms | ZB-624 |
| | | | DB-1701, VF-1701ms, CP Sil 19 CB, VF-1701 | |
| Rtx-1701 | 14% Cyanopropylphenyl/86% dimethyl polysiloxane (G46) | 280 °C | Pesticides, DB-1701R | ZB-1701, ZB-1701P |
| Rtx-200, Rtx-200MS | Trifluoropropyl methyl polysiloxane (G6) | 340 °C | DB-200, VF-200ms, DB-210 | _ |
| | 50% Cyanopropyl methyl/50% phenylmethyl polysiloxane | | | |
| Rtx-225 | (G7, G19) | 240 °C | DB-225ms, CP Sil 43 CB | _ |
| Rtx-440 | Proprietary Phase | 340 °C | RESTEK INNOVATIO | DN |
| Rtx-2330 | 90% Biscyanopropyl/10% cyanopropylphenyl polysiloxane (G48) | 275 °C | VF-23ms | _ |
| Rt-2560 | Biscyanopropyl polysiloxane | 250 °C | HP-88, CP Sil 88 | _ |
| Rtx-Wax | Polyethylene glycol (G14, G15, G16, G20, G39) | 250 °C | DB-Wax, Wax 52 CB | ZB-WAX |
| Stabilwax | Polyethylene glycol (G14, G15, G16, G20, G39) | 260 °C | HP-INNOWax, VF-WaxMS | ZB-WAXPlus |

Table II: Relative polarity and thermal stability are important considerations when selecting a GC stationary phase.

 * Maximum operating temperatures may vary with column film thickness.

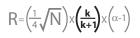
 Table III: Application-specific phases designed for particular analyses.

| Restek | Applications | Agilent | Supelco | Macherey-Nagel | SGE | Phenomenex |
|--|--|--|----------------|--|-------|------------|
| Rtx-Volatile Amine | Volatile amines | CP-VolAmine | _ | _ | _ | _ |
| Rtx-5Amine | Amines | CP-Sil 8 CB | _ | OPTIMA 5 Amine | _ | _ |
| Rtx-35Amine | Amines | _ | _ | RESTEK INNOVAT | ION | _ |
| Stabilwax-DB | Amines | CAM, CP WAX 51 | Carbowax Amine | FS-CW 20 M-AM | _ | _ |
| Stabilwax-DA | Free fatty acids | HP-FFAP, DB-FFAP, VF-DA, CP WAX58 CB, CP-FFAP CB | Nukol | PERMABOND FFAP,OPTIMA FFAP, OPTIMA FFAP Plus | BP-21 | ZB-FFAP |
| Chiral Columns | | | | | | |
| Rt-βDEXm, Rt-βDEXsm, Rt-βDEXse, Rt-βDEXsp, Rt-βDEXsa, Rt-βDEXcst, Rt-γDEXsa | Chiral compounds | _ | _ | _ | _ | _ |
| Foods, Flavors, & Fragrances | | | | | | |
| Rt-2560 | cis/trans FAMEs | HP-88 | SPB-2560 | _ | _ | _ |
| FAMEWAX | Marine oils | Select FAME | Omegawax | _ | _ | _ |
| Rtx-65 TG | Triglycerides | _ | _ | _ | _ | _ |
| Rxi-PAH | Polycyclic aromatic hydrocarbons (PAHs) | Agilent Select PAH | _ | _ | _ | _ |



| Restek | Applications | Agilent | Supelco | Macherey-Nagel | SGE | Phenomenex |
|--|--|--|-----------------------------------|-----------------------|---------|----------------|
| Petroleum & Petrochemical | | | | | | |
| Rt-Alumina BOND/CFC | Chlorinated fluorocarbons (CFCs) | _ | _ | RESTEK INNOVAT | ΓΙΟΝ | _ |
| Rtx-DHA | Detailed hydrocarbon analysis | HP-PONA, DB-Petro, CP Sil PONA CB | Petrocol DH | _ | BP1PONA | _ |
| Rtx-2887 | Hydrocarbons (ASTM D2887) | DB-2887 | Petrocol 2887, Petrocol EX2887 | _ | _ | _ |
| MXT-2887 | Hydrocarbons (ASTM D2887) | DB-2887 | Petrocol 2887, Petrocol EX2887 | _ | _ | _ |
| D3606 | Ethanol (ASTM D3606) | _ | _ | RESTEK INNOVAT | TION | _ |
| Rt-TCEP | Aromatics and oxygenates in gasoline | CP-TCEP | TCEP | _ | _ | _ |
| MXT-1HT SimDist | Simulated distillation | DB-HT-SimDis,CP-SimDist, CP-SimDist Ultimetal | _ | _ | BPX1 | ZB-1XT SimDist |
| MXT-1 SimDist | Simulated distillation | DB-HT-SimDis,CP-SimDist, CP-SimDist Ultimetal | _ | _ | _ | _ |
| MXT-500 SimDist | Simulated distillation | _ | _ | RESTEK INNOVAT | TION | |
| Rtx-Biodiesel TG, MXT-Biodiesel TG Clinical/Forensic | Triglycerides in biodiesel | Biodiesel, Select Biodiesel | _ | OPTIMA Biodiesel | _ | ZB-Bioethanol |
| Rtx-BAC Plus 1 | Blood alcohol testing | DB-ALC1 | _ | _ | _ | ZB-BAC1 |
| Rtx-BAC Plus 2 | Blood alcohol testing | DB-ALC2 | _ | _ | _ | ZB-BAC2 |
| Pharmaceutical | store aconor resulty | | | | | LU DACL |
| Rtx-G27 w/IntegraGuard | Organic volatile impurities (USP <467>) | | | | _ | |
| Rtx-G43 w/IntegraGuard | Organic volatile impurities (USP <467>) | _ | _ | | _ | |
| Rxi-624Sil MS | Organic volatile impurities (USP <467>) | DB-624,VF-624ms, CP-Select 624 CB | _ | OPTIMA 624 LB | BP624 | ZB-624 |
| Rtx-5 (G27) | Organic volatile impurities (USP <467>) | HP-5, DB-5,CP Sil 8 CB | SPB-5 | OPTIMA 5 | BP5 | ZB-5 |
| Stabilwax (G16) | Organic volatile impurities (USP <467>) | HP-INNOWax,CP Wax 52 CB,VF-WAX MS | Supelcowax-10 | OPTIMA WAXplus | _ | ZB-WAXplus |
| Environmental | | , | | • | | • |
| Rxi-5Sil MS | Semivolatiles | DB-5ms,DB-5msUI, VF-5ms,CP-Sil 8 CB | SLB-5ms | OPTIMA 5MS Accent | BPX5 | ZB-5msi |
| | Volatiles (EPA Methods | | | | | |
| Rtx-VMS | 8260, 624, 524) Volatiles | — DB-624.VF-624ms, | _ | RESTEK INNOVAT | TION | |
| Rxi-624Sil MS | (EPA Methods 624) Volatiles (EPA Methods | CP-Select 624 CB | _ | OPTIMA 624 LB | BP624 | ZB-624 |
| Rtx-502.2 | 8010, 8020, 502.2, 601, 602) Volatiles (EPA Methods | DB-502.2 | VOCOL | _ | _ | _ |
| Rtx-Volatiles | 8010, 8020, 502.2, 601, 602) Volatiles (EPA Methods | | VOCOL | _ | _ | _ |
| Rtx-VRX | 8010, 8020, 502.2, 601, 602) | DB-VRX | _ | _ | _ | _ |
| Rtx-CLPesticides | Organochlorine pesticides | _ | _ | RESTEK INNOVAT | ION | _ |
| Rtx-CLPesticides2 | Organochlorine pesticides | _ | _ | RESTEK INNOVAT | | _ |
| Rtx-1614 | Brominated flame retardants | _ | _ | RESTEK INNOVAT | | _ |
| Rtx-PCB | Polychlorinated biphenyl (PCB) congeners | _ | _ | RESTEK INNOVAT | | _ |
| Rxi-XLB | Polychlorinated biphenyl (PCB) congeners | DB-XLB,VF-XMS | _ | _ | _ | MR1, ZB-XLB |
| Rtx-OPPesticides | Organophosphorus pesticides | _ | _ | RESTEK INNOVAT | TION | _ |
| Rtx-OPPesticides2 | Organophosphorus pesticides | _ | _ | RESTEK INNOVAT | TION | _ |
| Rtx-Dioxin2 | Dioxins and furans | _ | _ | RESTEK INNOVAT | | _ |
| | Polycyclic aromatic | DB-17ms,VF-17ms, | | | | |
| Rxi-17Sil MS | hydrocarbons (PAHs) | CP-Sil 24 CB | _ | OPTIMA 17 MS | BPX50 | ZB-50 |





Select Column Film Thickness and Column ID Based on Retention Factor

Once you have chosen the stationary phase, you need to determine which column film thickness and inner diameter combination will give the retention factor (k) needed for optimal resolution and speed. Retention factor is sometimes referred to as capacity factor, which should not be confused with sample loading capacity.

The retention factor (k) of a column is based on the time an analyte spends in the stationary phase relative to the time it spends in the carrier gas. As a general rule, the thicker the film and the smaller the inner diameter, the more an analyte will be retained. Note that as temperature increases k decreases, so at higher temperatures analytes stay in the carrier gas longer and are less retained.

In practice, if the value of k is too large, the peak will broaden, which can reduce resolution by causing peaks to overlap or coelute. Narrow, symmetrical peaks are important to maximizing resolution, so the goal is to select a column with a sufficient retention factor, such that resolution occurs and peak shape does not suffer. Once the proper stationary phase is selected, column film thickness, column inner diameter, and elution temperature should be optimized to produce an acceptable retention factor.

Film Thickness

Film thickness (μ m) has a direct effect on both the retention of each sample component and the maximum operating temperature of the column. When analyzing extremely volatile compounds, a thick film column should be used to increase retention; more separation is achieved because the compounds spend more time in the stationary phase. If analyzing high molecular weight compounds, a thinner film column should be used, as this reduces the length of time that the analytes stay in the column and minimizes phase bleed at higher elution temperatures. Use Figure 3 to select the best film thickness for your application. Note that as a general rule, the thicker the film, the lower the maximum temperature; exceeding the maximum temperature can result in column bleed and should be avoided.



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The sample loading capacity of the column also must be considered; if the mass of the target analyte exceeds the sample loading capacity of the column, loss of resolution, poor reproducibility, and fronting peaks will result. A larger ID column with thicker film is recommended for higher concentration samples, such as purity analysis, to minimize sample overload.

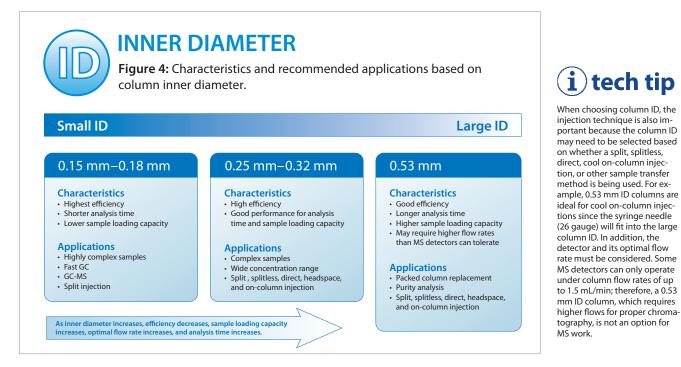


Remember, when changing either film thickness and/or the temperature program, you must reconfirm peak identifications as elution order changes can occur.



Inner Diameter (ID)

Column ID does not have as great an effect on retention factor as film thickness does. However, when selecting column ID with retention factor (k) in mind, a general rule of thumb applies; smaller ID columns produce higher retention factors compared to larger ID columns. This is due to less available mobile phase (carrier gas) volume in the column. Because smaller ID columns produce higher k values, they are more suited towards complex sample analysis where a range of low to high molecular weight compounds may exist in the sample (Figure 4). Keep in mind that both ID and film thickness should be optimized together to produce the best resolution and peak shape.



Phase Ratio (β)

The relationship between column inner diameter and stationary phase film thickness is expressed as phase ratio (β). If a good separation has been achieved on a larger diameter column and a faster analysis is desired, this can often be accomplished by reducing the inner diameter of the column without sacrificing, and sometimes even improving, separation efficiency. To maintain a similar compound elution pattern when narrowing column inner diameter, film thickness must also be changed. By choosing a column with a similar phase ratio, it will be easier to translate your application to the new column. Phase ratios for common column dimensions and the equation for β are given in Table IV. As shown here, an analyst wanting to decrease analysis time could switch from a 0.32 mm x 0.50 µm column (β = 160) to a 0.25 mm x 0.25 µm column (β = 250) and obtain a very similar separation upon proper method translation. Importantly, column inner diameter and stationary phase film thickness show a combined effect when it comes to sample loading capacity, which is decreased as column inner diameter and film thickness are reduced. It may be necessary to inject a lower sample amount in this case.

Table IV: Phase ratio (β)* values for common column dimensions. To maintain similar separations, choose columns with similar phase ratios when changing to a column with a different inner diameter or film thickness.

| | | | F | ilm Thickness (d _f |) | | |
|-----------|---------|---------|---------|-------------------------------|--------|--------|--------|
| Column ID | 0.10 µm | 0.25 µm | 0.50 µm | 1.0 µm | 1.5 µm | 3.0 µm | 5.0 µm |
| 0.18 mm | 450 | 180 | 90 | 45 | 30 | 15 | 9 |
| 0.25 mm | 625 | 250 | 125 | 63 | 42 | 21 | 13 |
| 0.32 mm | 800 | 320 | 160 | 80 | 53 | 27 | 16 |
| 0.53 mm | 1,325 | 530 | 265 | 128 | 88 | 43 | 27 |

*Phase ratio (β) = radius/2df (Note: Convert variables to the same units prior to calculation.)

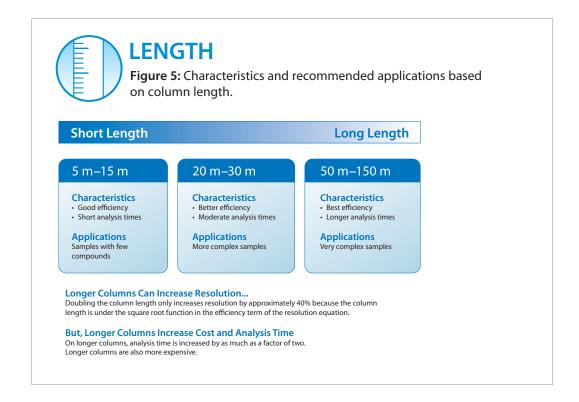




Consider Efficiency when Choosing Column Length, Column ID, and Carrier Gas

Column Length

Capillary GC columns are made in various lengths, typically 10, 15, 30, 60, and 105 meters, depending on the inner diameter. Longer columns provide more resolving power than shorter columns of the same inner diameter, but they also increase analysis time and should be used only for applications demanding the utmost in separation power. Column length should only be considered once the stationary phase has been determined. This is because separation factor has the greatest effect on resolution, and it is maximized through proper stationary phase choice for the compounds of interest. Doubling the column length (e.g., 30 m to 60 m) increases resolution by approximately 40%, while analysis time can be twice as long. In addition, longer columns cost more. Conversely, if a separation can be performed on a shorter column (e.g., 15 m versus 30 m), then both analysis time and column cost will be less. Figure 5 summarizes the characteristics and general application parameters for a range of typical column lengths.



Inner Diameter (ID)

Compared to larger ID columns, smaller ID columns generate more plates per meter and sharper peaks, leading to better separation efficiencies. When more complex samples need to be analyzed, smaller ID columns can produce better separation of closely eluting peaks than larger ID columns. However, sample loading capacities are lower for smaller ID columns. Smaller ID columns, especially those at 0.18 mm and less, demand highly efficient injection techniques so that the column efficiency is not lost at the point of sample introduction. Column characteristics based on ID are presented in Table V.

Generally speaking, a 0.25 mm column will produce the most efficient sample analysis while simultaneously considering analysis time and sample loading capacity. For these reasons, in combination with its relatively low outlet flow, it is also the best column choice for GC-MS work.

| | | | Column Inner D | iameter (mm) | | |
|------------------------------|--------|-------|----------------|--------------|-------|-------|
| Characteristic | 0.10 | 0.15 | 0.18 | 0.25 | 0.32 | 0.53 |
| Nitrogen flow (mL/min) | 0.2 | 0.3 | 0.3 | 0.4 | 0.6 | 0.9 |
| Helium flow (mL/min) | 0.6 | 0.8 | 1.0 | 1.4 | 1.8 | 3.0 |
| Hydrogen flow (mL/min) | 0.7 | 1.1 | 1.3 | 1.8 | 2.3 | 3.7 |
| Sample loading capacity (ng) | 2.5 | 10 | 20 | 50 | 125 | 500 |
| Theoretical plates/meter | 11,000 | 7,000 | 6,000 | 4,000 | 3,000 | 2,000 |

Carrier Gas Type and Linear Velocity

Carrier gas choice and linear velocity significantly affect column separation efficiency, which is best illustrated using van Deemter plots (Figure 6). The optimum linear velocity for each gas is at the lowest point on the curve, where plate height (H) is minimized, and efficiency is maximized. As seen in Figure 6, the optimum linear velocities differ among common carrier gases.

Nitrogen provides the best efficiency; however, the steepness of its van Deemter plot on each side of optimum means that small changes in linear velocity can result in large negative changes in efficiency. Compared to nitrogen, helium has a wider range for optimal linear velocity, but offers slightly less efficiency. In addition, because of its optimum velocity being faster, analysis times with helium are about half those when using nitrogen, and there is only a small sacrifice in efficiency when velocity changes slightly. Of the three common carrier gases, hydrogen has the flattest van Deemter curve, which results in the shortest analysis times and the widest range of average linear velocity over which high efficiency is obtained.

Regardless of the type of gas used, the carrier gas head pressure is constant during column temperature programming, whereas the average linear velocity decreases during the run. For constant pressure work then, the optimal linear velocity should be set for the most critical separations. More commonly today, electronic pneumatic control (EPC) of carrier gas allows for constant flow or even constant linear velocity, which helps maintain high efficiency throughout a temperature programmed run.

Another consideration for carrier gas type that is important, even if not directly related to column efficiency, is whether a mass spectrometer (MS) is used as a vacuum-outlet detector for GC. In almost all cases, helium is the carrier gas of choice, not only for its chromatographic efficiency, but also because it is easier to pump than hydrogen. Hydrogen can be reactive in MS sources, leading to undesirable spectrum changes for some compounds. Nitrogen is typically not a carrier gas option for GC-MS, as it severely reduces sensitivity.

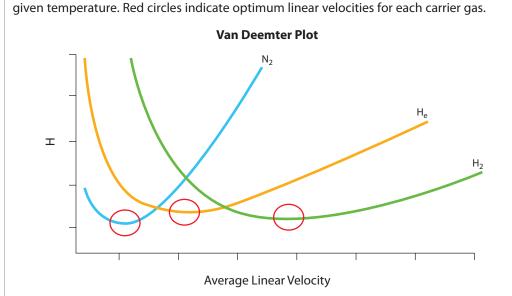


Figure 6: Operating carrier gas at the optimum linear velocity will maximize efficiency at a



When changing carrier gas flow rates you must reconfirm peak identifications as elution order changes can occur.



GC TROUBLESHOOTING TIPS

Basic Steps

Follow these basic troubleshooting steps to isolate problems related to the sample, injector, detector, and column. Check the obvious explanations first and change only one thing at a time until you identify and resolve the problem.

Check the Obvious:

- Power supply
- Gas purity
- Electrical connections
- Signal connections
- Gas flows
- Temperature settings
- Syringe condition
- Sample preparation
- Analytical conditions

Identify the Cause:

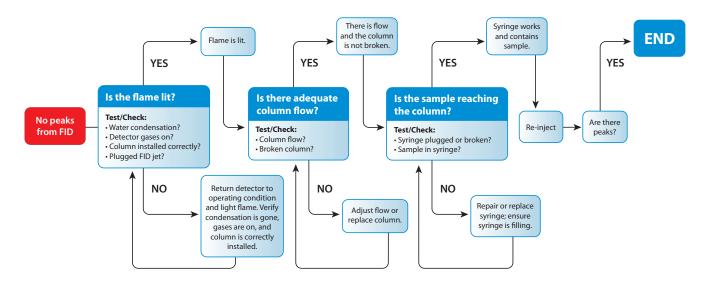
- Define the problem clearly; for example, "Over the last 4 days, only the phenols in my sample have been tailing."
- Review sample and maintenance records to identify trends in the data or problem indicators, such as area counts decreasing over time or injector maintenance not being performed as scheduled.
- Use a logical sequence of steps to isolate possible causes.

Document Work and Verify System Performance:

- Document all troubleshooting steps and results; this may help you identify and solve the next problem faster.
- Always inject a test mix and compare to previous data to ensure restored performance.

Example Troubleshooting Sequence

An analyst observed that no peaks appeared during a GC-FID analysis. The flowchart below shows a logical progression of steps that can be used to identify the cause and correct the problem.



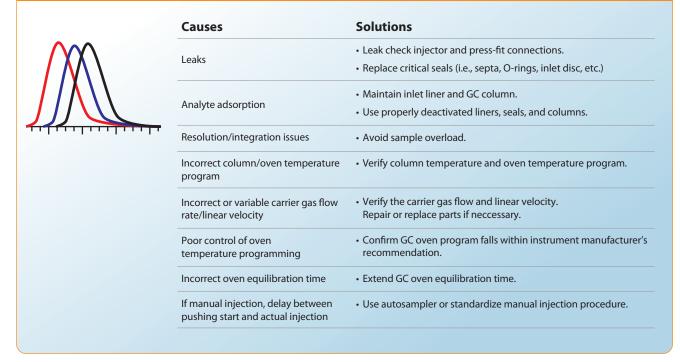


Symptoms and Solutions

Good chromatography is critical to obtaining accurate, reproducible results. Coelutions, asymmetric peaks, baseline noise, and other issues are common challenges in the GC laboratory. These analytical problems and others can be overcome by troubleshooting your separations using the tips below.

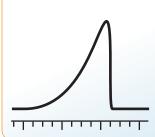


Poor Retention Time Reproducibility





Fronting Peaks



| Causes | Solutions |
|-------------------------------|---|
| Incompatible stationary phase | Choose appropriate stationary phase. |
| Column overloading | Reduce amount injected, dilute sample. Increase column inner diameter and/or film thickness. |

Tailing Peaks

| • | Causes | Solutions |
|---|---|--|
| | Adsorption due to surface activity or contamination | Use properly cleaned and deactivated liner, seal, and column. Trim inlet end of column. Replace column if damaged. |
| | Adsorption due to chemical composition of compound | Derivatize compound. |
| | Leak in system | Check for leaks at all connections, replace critical seals if needed. |
| | | Minimize dead volume. |
| | Installation issues | Verify that the column is cut properly (square). |
| | | Verify correct installation distances. |

| | Split | Peaks |
|---|--|---|
| | Causes | Solutions |
| Λ | Mismatched solvent/stationary phase polarity | Adjust solvent or stationary phase to allow wetting. |
| | Incomplete vaporization | Add surface area, such as wool, to the inlet liner to enhance vaporization. |
| | | Use proper injector temperature. |
| | Sample loading capacity exceeded | Inject less sample (dilute, use split injection, reduce injection volume). |
| | Fast autosampler injection into open liner | Use wool or slow injection speed. |



Carryover/Ghost Peaks

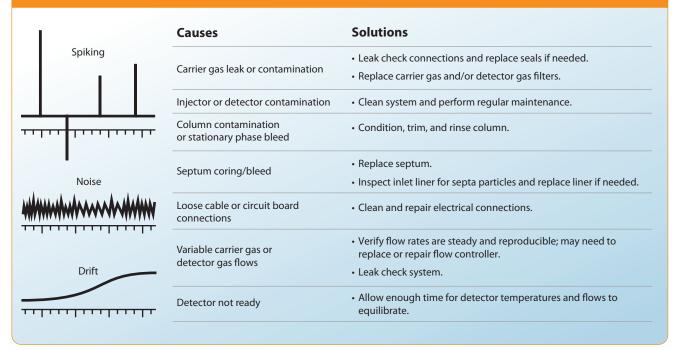
| | Causes | Solutions |
|-------------|------------------------------|--|
| Injection 1 | Contaminated syringe or | Replace rinse solvent. |
| | rinse solvent | Rinse or replace syringe. |
| | | Inject a smaller amount. |
| | | Use a liner with a large internal diameter. |
| | | Increase head pressure (i.e., flowrate) to contain the vapor cloud |
| | Backflash (sample volume | Use slower injection rate. |
| | exceeds liner volume) | Lower inlet temperature. |
| | | Increase split flow. |
| Injection 2 | | Use liner with packing. |
| | | Use pressure-pulse injection. |
| | Last analysis ended too soon | Extend analysis time to allow all components and/or matrix interferences to elute. |

High Bleed Causes **Solutions** Improper column conditioning • Increase conditioning time and/or temperature. • Trim column and/or heat to maximum temperature to remove contaminants. Contamination • Replace carrier gas and/or detector gas filters. • Clean injector and detector. Check for oxygen leaks across the entire system and replace seals Leak in system and oxidation of and/or filters. stationary phase • Replace column.





Unstable Baseline (Spiking, Noise, Drift)

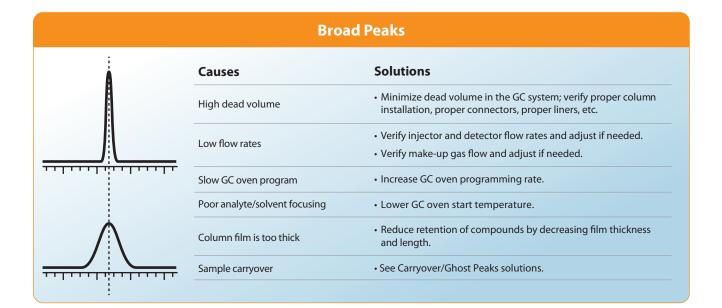


Response Variation

| | Causes | Solutions |
|---|---|---|
| | | Check sample concentration. |
| | Sample issues | Check sample preparation procedure. |
| | | Check sample decomposition/shelf life. |
| | Syringe problems | Replace syringe. |
| | Synnge problems | Check autosampler operation. |
| ٨ | Electronics | Verify signal settings and adjust if needed. |
| | Electronics | Repair or replace cables or boards. |
| | Dirty or damaged detector | Perform detector maintenance or replace parts. |
| | Flow/temperature settings wrong or variable | Verify steady flow rates and temperatures, then adjust settings and/or replace parts if needed. |
| | Adsorption/reactivity | Remove contamination and use properly deactivated liner, seal, and column. |
| | Leaks | Check for leaks at all connections and repair connections as needed. |
| | | Verify injection technique and change back to |
| | Change in sample introduction/injection | original technique. |
| | method | Check that split ratio is correct. |
| | | Verify that the splitless hold time is correct. |



| Solutions Plugged syringe; clean or replace syringe. |
|--|
| Plugged syringe; clean or replace syringe. |
| |
| Verify there is sample in the syringe. |
| Injecting into wrong inlet; reset autosampler. |
| Verify carrier gas is flowing. |
| Replace column. |
| • Re-install column. |
| Signal not recorded; check detector cables and verify that detector is turned on. |
| Detector gas turned off or wrong flow rates used; turn detector on and/or adjust flow rates. |
| |



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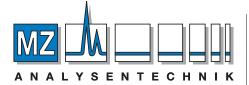
Simplifying Column Selection



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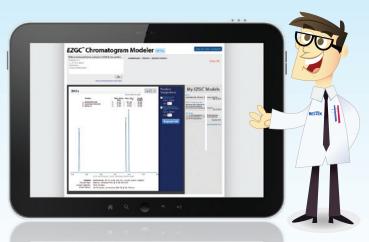


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